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(54) WASHING METHOD FOR SILICON WAFER

(57) Abstract:

PURPOSE: To obtain a silicon wafer having high cleanliness by washing this silicon wafer by using an aq. soln. contg. hydrogen fluoride and contg. a specific oxidizing agent as a detergent.

CONSTITUTION: The aq. soln. contg. 0.1 to 20wt.% hydrogen fluoride and contg. the oxidizing agent described below as the detergent is used at the time of washing the silicon wafer. (i) 0.5 to 25wt.% sulfuric acid or (ii) 0.05 to 10wt.% hydrogen peroxide or (iii) bubbles of an oxidative gas are used as the above mentioned oxidizing agent. Gases contg. oxygen and nitrogen suboxide are usable as the oxidizing gas. Ultrapure water is used as the solvent. The evaporation of the hydrogen fluoride and the water and the evaporation decomposition of nitric acid are accelerated and the compsn. of the washing liquid may deviate from the range of this method if the washing temp. is increased to more than a necessary high temp. Further, the heating up takes time and such may drastically impair workability and, therefore, the heating up to 80°C is more preferable.

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の発明の名称

シリコンクエハの洗浄方法

创特 題 平2-3386

願 平2(1990)1月12日 **多**出。

山口県光市大字島田3434番地 新日本製鐵株式會社光製鐵

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し、及男の名称

シリコンウェハの改修方法

- 2.特許請求の範囲
- (1) クリコンウェヘを沈沙するに関し、0.1 ~:20 **産量%の多化水果を含有し、かつ酸化剤として、** とすることを特殊とするシリコンウェハの佐身方
- (2) シリコンウェハを失声するに終し、9.95~18 重量%の赤化水炭を合存し、かつ酸化剤として 9.95~10通星%の過안化水架を含有する水溶液を 洗神波とすることを特徴とするシリコンウェハの **洗炉方法**。
- (3) グリコンウェハモ技術するに終し、6.05~10 重量%の現化水溝を含有し、かつ酸化剤として酸 化性ガスの気迫を超入せしめた水溶液を抵外設と することも特束とするシリコンクェハの洗券方 住.
- 3.発明の詳細な説明

産業上の科用分野

東京都平代田区大手町2丁目6番3号

本発明は、シリコンウェハの表面を高清浄な状 無にするための政権方法に関するものである。 従来の技術

* 近年,デバイスの商集積化に停って、その基数 となるシリコンウェへの表面をより一般循序化す

シリコンクェへの表面に、シリコン粒子や虚句 の世枝千行英句質(パーティクルとも言われる) が存在すると、デバイス配線の路線やショートの 質因となり、益非金属等の金属系汚換物類がある と、酸化酶超級器欠陥の発生やライフタイムの低 下といった問題が生じる。このため、これの形象 粉質を終去するための抗疫が行われるが、発移の 際に拘禁されることも避けなければならない。

供食のシリコンウェハの洗浄方法としては、 ②希弥殿水溶液で洗浄する方法。 ②塩酸コたは硫 蘇と遊戯化水器との混合水彩液で沈がする方法。 および匈アンモニアと遊跡化水裏の混合水母級で **徒降する方法が行われている。これらる茂浄法で**

注册平3-208900 (2)

使用される独海療には、敵様子特殊物質や全民選 存集物質を極力過酸した温齢度の薬品類や水が使 用されている。

従来の税券方法のうち、①はシリコンウェハ表 商に造名10入程度の厚さで存在する自然酸化緩を 溶解する能力を有し、飲化額中の企業系汚染物質 の除去効果は高いが、単粒子汚染物質の低級は無 しいという問題がある。

少は増設または複融が持つ全民系汚染物質に対 する足球解能力を利用したものであるが、酸化設 をお解する能力がない。このため、酸化設上の金 展系汚染物質を飲出する効果は高いが、酸化設中 や酸化設とシリコンの界面に存在する金属系汚染 物質を除去する効果は低い。

毎はシリコン自身を増加する働きがあるため、 その上に存在する金属系汚染物質を除去する効果 は高いが、塩基性の洗浄液中で生成する砂化膜は 洗浄液中の金属系汚染物質等を取り込み易いとい う性質があり、シリコンウェハが再行染される可 能性が高い。しかし、この方法は微粒子の論表薄

したがって、スタイトニッチ生でもシリコンウェ ハの高級強化には眩界があると言わざるをえな い。

毎朗が解決しようとする課題

太陽明は、シリコンウェバを抜降するに難して、Pa等の会議市所築物質および競技子背換物質を振めて低級し、健化諸超級層欠略の発生やライ

泉が高いため、ウェハメーカーやデバイスメーカーで広く利用されている。

また、上部従来法の問題点を解消する方法として、60重量%の組織と 4.1党産%以下の赤化水炭の混合水溶液中にシリコンケェハを放棄して代券するステイトエッチ法と呼ばれる方法が選案されている。(Qitum Takizawa ら、"Bateaded Abslrocts of Solid State Beriess and Materials"、1988年、P.475)。

しかし、幸運体別グレードと呼ばれる最高純度の前肢でも、ppb オーダーまたはサブppb オーダーの会議系持険価値にとえば起、Ca、Ca、Fa、R、Na、2a等が含まれているので、86会量がもの路底の硝酸を含む旋炸級中の会議系得無価質の選股は高く、また石英ガラス製の洗浄機を使用すると石灰ガラス中の金属不純物が溶出して、その値度はますます為まる。

をして、高級設的酸の強い酸化力でシリコン ウェハの裏部に酸化膜が形成され、洗券扱中の金 網系形染物質が酸化膜中に取り込まれ易くなる。

フタイムの低下といった品具問題がなく、かつデバイスにした場合の電気特性の労化もない高額枠 信のシリコンヴェハを得ることを目的とする。 課題を解決するための手段および作用

水苑明の更旨はつぎのとおりである。

- (1)、シリコンウェハを記録するに終し、 8.1~20 金量%の形化水災を合おし、かつ能化剤として 8.5~25度量%の明酸を含有する水溶液を洗浄症 とすることを特徴とするシリコンフェハの洗浄力 法。
- (2) シリコンウェハを沈然するに関し、6,65~16 主量労の亦化水溝を含有し、かつ酸化剤として 8.65~10度量労の過酸化水溝を含有する水溶液を 洗浄液とすることを特別とするシリコンウェハの 洗浄方益。
- (4) シリコンウェハを洗浄するに関し、0.05~19 重量%の鼻化な器を合称し、かつ酸化物として酸 化性ガスの気泡を収入せしめた水溶療を洗浄液と することを特徴とするシリコンウェハの洗浄方 法。

销局平3-208900 (3)

本発明法において、党枠設中の市化水業、消費 および過酸化水素の濃度は、それぞれ即、BNO3、 および助のとしての重更分である。請求項(3) に おいては、酸化性ガスとして酸素および亜酸化食 業 (一般化二氢素) 等を含むガスを使用すること ができる。また、溶媒としては熔純水を使用する。

湖でかつ品散化木果が9.05労星労決損だと、金屋系売執知の終去効果が不充分である。 お化水类の面层を増して10年最労を越えると、ショコンウニハの液面に散粒子汚染物質が増加する傾向が 届められる。また過酸化水準の濃度を増して10重 最为を結えると、シリコン東面のエッチング量が 過六になってウニハ炭酸が増れて参った状態になる。そして、非化水素が10重量労以下でかつ過酸化水素が10重量労以下では、薬剤から混入する不能物の過度は実異上問題ない。

したがって、売化水煮の濃度を0.05~18萬益%、 過酸化水果の濃度を0.05~10重量%とした。 なお、洗浄温度については、80℃を終えると洗浄むらが完じて熟過建設のシリコンウェハ表面にピット状火路を到起するおそれがあるので、80℃以下とするのが望ましい。

請求項(3) において、先化水男が8.05億量% 最 機でかつ酸化性ガスの無難を収入させない場合は 金屋不朽染物質の鉄去効果が不充分である。 お化 木実の濃度を増して10番量労を越えると、シリコ 請求役(1) において、発化水素が 6.2 重異名米 調でかつ前限が 6.5 重量粉末機だと、金属系符染 物質の快去効果が不充分である。非化水素の複変 を適して20重量粉を越えると、シリコンウェハの 表際に散粒子行染物質が増加する傾向が認められ る。また硝酸の資度を増して25重量粉を超える と、シリコン表面のエッチング量が過大になって ウェハ表面が流れて劣った状態になる。そして、 邪化水素が20重量粉以下でかつ納度が25重量粉以 下では、薬剤から超入する不動物の濃度は変質上 問題ない。

したがって、多化水黄の濃度を 6.1~26質量光、 研飲の濃度を 0.6~25速量光とした。水粉、枕井 湿度については、必要以上に高温にすると悪化水 素粉よび水の蒸気や消費の蒸発分解が促進されて 投浄液の組成が水発明の結節から外れるおそれが あり、さらに昇湿に時間がかかり作業性を楽しく 損なうようになるので、90℃以下とするのが望ま しい。

請京項(2)において、弗化水器が8,05重量分果

ンウェハの製館に教柱子行集物質が増加するとともにエッチング量が過去になってウェハ表題が荒れる。そして、単化水楽が10強量%以下では超弱から超入する不純物の譲渡は実費上問題なく、また離化性ガスは不純物譲渡の描めて低い高齢度のものが比較的容易に持られるので問題ない。

したがって、売化水宮の資度を9.05~10重量が とし、鉄化畑として飲化性ガスの気泡を殺人せし めることとした。なお、鉄神温度については、 80でを越えると供待ひ方が生じて熱処理後のシリ コンウェハ表面にピット状欠陥を誘起するおそれ があるので、40で以下とするのが気ましい。

残物故に酸化性ガスの気想を潜入せらめるに は、携帯物内にガス導入管を入れてパブリングさ せるか、あるいは発体器の底部にガス吸出孔を設 けてパブリングさせる等の公知の手及を禁用する ことができる。

本発明法によれば、シリコンと矛葉イオンとの 間に生じるシリコンのアノード溶解反応と、酸化 剤の起こすカソード反応とが電気化学的にカップ

销期平3-208900 (4)

ルして決められる異女鬼位がアノード部になるので、シリコンウェハ表因の金属系乃染物質が除去されやすい。

北発明社の範囲の参案イオンを含む強敵性の水 格兼中ではシリコン酸化物からなる不明整収穫が 化学的または電気化学的に容易し、シリコンウェ 小美額が初の状態になるため、酸化剤が必要量数 加されて腐食電位がアノード側になるとウェへ表 面の金属系列染物質が容易に除去される。

なお、太契明法において、抗移政の成分として 上記以外のもの例えば本化アンモニウム学の協規 を洗浄確に抵加したとしても洗浄能力が損なわれ ることがない。

さらに、本発明法において、従来公知の批准法 と組み合わせて行ってもよい。例えばアンモニア と過触元太美の退合水溶液で批準し、さらに効果 酸水溶液で洗浄した後、本発明法により洗浄する とより効果的である。

災地例

(1) 結束項(1) の異範例

水性であるかを巨視により科定し、疎水性であるものを〇田、やや緑水性であるものを△田・親水性であるものを△田・親水性であるものを×甲で表示した。森水性であればシリコンウェハの表面にはシリコンの酸化物すなわら酸化脱が存在しないことを示す。

さらに、光学類数鏡によりウェハ表面のピット 状久皓の有無を観察して表示した。ピット状欠略 なしは、ニッチング量が過正で極めて平滑な鏡面 状態の表面を有していることを示している。

第1表において、比較例のHo.1およびNo.15 は 売化水素が少ないため毎にFeおよびGoの残存量が 多く、四じくNo.8およびNo.14 は悪化水実が多す ざるためピット状欠陥が生じるとともに観察子符 染物質が成存した。また、比較例のPo.19 および No.26 は発散が多すざるためピット状欠陥が生じ た。

世来例の30.21 ステイトエッチ法は350:89差 量労、3F:0.1意量光の水溶液で改作したものであるが50の除去効果が低い。86.22 アンモニア過酸 化水果法は 80:4.1度量%、50:4.4定量%の水 約 270×19 to a to a 2/cm² の Cr. 約 240×10 to a to a 3/cm² の Ge. 約 2230×10 to a to a 3/cm² の Po 5 よび約 314×18 to a 109 5/cm² の 門により表面が行 気されたシリコンウェハを、第1表に示す各種洗 確確に被接して洗掉した結果を開張に示す。洗涤 技のシリコンウェハは、近ちに超減水中で5分間 以上の淡水水洗を2回行い、スピンドライヤーにより転送した後、製画の汚染金属の分析に共した。

分析性、過剰的融資域によりかりコンフェハの 支給1月四を化学ニッチングして溶解し、放棄解 銀中の会議元素機成をフレームレス原子吸光光度 分析法により足量した。なお、液中のIDは分析定 是下限以下であることを示し、Crは 9.1×10¹⁰ atoma/cm² 未満、CoおよびFeは 9.2×10¹⁰ atoma/cm² 未満、Niは 2.8×10¹⁰ atoma/cm² 未満である。

ウェハ表面の数粒子は、ウェハ表面景粒子計算 製量により背定し、18個/ウェハ以下を〇〇、 10個/ウェハ磁を×印で表示した。

また、花林袋のウェハ表面が疎水位であるか製

溶液で洗浄したものであるが、多種飲料法の中で最も全度系の飲物質の飲去効果が低く、特にF4の飲去効果が低く、特にF4の飲去効果が低い。No.25 塩酸過酸化水果法及 EQ :3.1 鱼量が、込み:4.4 重量がの水溶液で洗浄したものであり、全属系得染物質除去のために現在最も多用されている洗浄法であるが、水道明例に比べて供応F4の飲去効果が低い。

太是明別(1) は、何れもシリコンウェハ表面の 単粒子汚染物質および全属系汚染物質が描めて低 減され、気炉染の表面にピット状欠態もない。ま た染疹後の家面には酸化酸が存在せず、硬水性の 支面状態になっている。これは、洗浄中に酸化聚 が形成されてその中に洗浄板中の金属系汚染物質 が取り込まれるという洗浄による再汚染が、本発 明別(1) では生じていないことを意味する。 121 請求項(2) および請求項(3) の実施例 約18×10 ** atama/om² のCr. 約 118×15 ** atama/cm² のCo. 約 110×18 ** atama/cm² のPeお よび約21×10 ** atama/cm² の別により表面が汚染

されたシリコンウェハモ、第2次に示す各種技権

特局平3-208900 (6)

液に投設して独物した結果を同変に示す。沈彦技のシリコンウェハは突結例[1] と同様に水洗蛇様し、金属系拐換物質の分析、数粒子汚染物質の批 定対よびピット状欠略の類点を行った。その結果を終2表に示す。

本発明の請求項(2)の実施制である本発明例 (2)および請求項(3)の実施例である本発明例 (3)は、何れも金属系行染物質および散粒子行験 物質が極めて複談され、かつピット状欠陥もない

比較例のNc: 8は発化水業および過酸化水業が少ないため、また比較例のNo. 9は悪化水業が少ないためCr. Ca. Feの残容量が多い。比較例のNo. 15は酸化剂の量が少ないためCr. Ca. Feの残容量が多い。また、比較例のNo. 16、No. 17、No. 19のように発化水業や過酸化水素の量が多すざると、ピット状欠陥が現れたり散粒子汚染物質が増加したりする。

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54	0.80	19-6	なし	380	25	KD .	. MD	¥9	NB.	0	なし	0	本是明例1
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10	6.50	6.00	* 1	360	8 0 [ND.	No	砌	MO	0	# L	•	木类明例1
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12	15.1	6 . 10.	0.15	300	25 ·	EĐ	ND.	挪	M	0	# L	O ·	水烃明例 1
13	15.0	20.0	# L	300	25	68	RD	, AD	- AD	0	なし	0	本発明例1
14	-15.0	30.0	4 L	100	25	MB	MB .	· ND.	96	Ö.	B 9	×	比較例
15	25.0	. 0.05	2 6	300	25	ND.	1.8	3,3	DiD .	/ X	# L	0	比较例
18	25.0	.0.10	# 6	200	. 25 .	MD	NĐ	MD	MB	0	a .	. 0	木発男例 1
17	25.0	\$-60	* L	300	25	100	BB	12	'ND	. 0	# 6	· 0	水瓷明例1
18	25.0	10.0	& L	895	25	ind	DX	NB	,XD	0	# L	o .	本発明例1
18	30.0	5.60	なし	\$00	25 .	88	850	NB	. AD	0	b 9	0	比较何
20	78.0	20.0	なし	386	25	FE	19	DB	EQ.	Ġ.	A 4	Ö	比较的
21	スグイト	エッチだ		309	70	ND .	2.8	34	118	×	& L	0	使来例
.55	アンモニ	7 选款化	水黄花	860	.83	2.7	2.4	77	HD	×∵	# L	0	关来例
28.	运船沿廊	化水囊法		600	.80	HD :	n.O.	15	NO.	. x	# L	0	税采 第
لبيا		·											

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数 2 美

Bo	13F	B,0 t	住化性ガスの組成 (3)	帝三成分	选 持	报器		· B · cto			7 h	菜粒子	区分	
	(2)	(\$)	(4)		(\$£C)	(30)	Gr	Fe	. \$1	Cu	状欠胎		秀獎	
61	4.85	1.00	≈ L .	*L	800	25	. KD	·ND	ND.	ND	4	し	0.	未発明例(2);
92	8.51	0.18	æL	a L	808	25	RD	ND	"MD"	NO.	#	L	• •	本竞男份(2)
83	0.19	2.01	at L	αL	600	25	CK.	m	MD.)AD	4	しし	•	太英男妇(2)
96	50	0.12	#1	なし	690	25	ND	GK	119	жD	*	L.	0	本竞明册(2)
65	1.05	9.11	· #b.	なし .	360	- 25	ND .	GN	#8)(D)	#	Ł	0	木尧明例(2)
08	1-66	1.07	*L	MB.F 0.10%	240	25	ER	MD .	MD	MD	#	Ł	\Q	本発明例(2)
07	0.93	5.00	a L	なし .	120	25	ЖÐ	MĐ)XO	. MD	#	L	. 0	本竞明例(2)
98	6.63	8.04	#b	なし	688	25	\$.2	6-6	XID	5.3	#	Ł	0	比較例
69	0.01	1.00	ない	#L.	600	25	13.2	29.4) D	12.4	*	L	0	比較例 :
10	0.10	0-29	æt,	まし	\$00	49	30	#D	XD	119	*	L	. 0	木英明例(2)
21	D. 65	なし	pars 02	46	608	25	ND	MB	ΕN	MĐ	*	L	O ·	木尧明例(3)
12.	9.15	まし	80202-2024x	QL	800	25	. מע	₩Đ	.ND	IID	~	L	.0	木克男例(3)
13	1.01	2 L	26302+803N2	NEAF 0.19%	380	28	MED	MD	NB	MD .	な	L	0	太월明份(1)
14	0-02	æ . t	20 BIBS	\$ L	380	25	5.6	45.8	₩B	7.9	本	ŀ	0	比較例
15	0.15	0.01	なし	#L	· 60 0	25	8.8	12.4	HD	0-4	Æ .	し	٥	比較例
!8	21.0	7.05	・なレ	ά ኒ	600	25	199	柳	M 9	粒	*	6	×	比較多
15	5.25	10.2	#↓ ・	æL	609	. 25	MÐ	翻	#\$)	MD .	**	ñ	0	比较例
13	11.2	# L	bate 02	. al	698	. \$2	MB	WB .	# 3	10	*	43	X .	比較例
13	1.00	4 L	202N;O+882N2	なし	- B08-	36	MD	MĐ	#6	CN	*	し	0	太是明确(2)

発明の対策

本発明はによりシリコンクェハを洗浄すると、 会経系汚染物質および教授子汚染物質がともに確 めて低減された高高浄度のシリコンウェハが得ら れ、酸化論起放開欠低の発生やライフタイムの係 下といったシリコンクェハの品質係下が回避され るとともに、ICや LSIなどの高気積化したデバイ スに使用した場合の電気物性劣化のおそれも回避 される。

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Specifications

Name of Invention

Cleaning Method for Silicon Wafer

- Claims
- A method for cleaning a silicon wafer is characterized by a cleaning liquid comprised of an aqueous solution that contains 0.1-20 wt% hydrogen fluoride during the silicon wafer cleaning process, along with 0.5
- 25 wt% nitric acid that is used as an oxidizing agent.

- (2) A method for cleaning a silicon wafer is further characterized by a cleaning liquid comprised of an aqueous solution that contains 0.05 10 wt% hydrogen fluoride during the silicon wafer cleaning process, along with 0.05 10 wt% hydrogen peroxide that is used as an oxidizing agent.
- (3) A method for cleaning a silicon wafer is further characterized by a cleaning liquid comprised of an aqueous solution that contains 0.05 10 wt% hydrogen fluoride during the silicon wafer cleaning process, along with oxidizing gas bubbles that are mixed into the solution to be used as an oxidizing agent.

3. Detailed Description of the Invention

Industrial Field of Application

This invention pertains to a cleaning method designed to provide a high level of cleanliness along the surface of a silicon wafer.

Prior Art

In recent years, the high level of integration within devices has brought a strong demand for an improved level of cleanliness along the surface of the silicon wafers that are used as substrates for these devices.

When minute contaminants (also referred to as particles) exist along the surface of a silicon wafer, such as silicon particles, dust, etc., this can result in disconnections and shorts along the wires within a device, and in cases where metallic contaminants exist such as transition metals, other problems can arise such as the occurrence of defects along the oxidation inductive lamination layer, as well as a drop in the lifetime of the device. For this reason, when a cleaning process is conducted for the purpose of removing these contaminants, it is also necessary to prevent contamination during the cleaning process.

Recently, the following methods have been used for cleaning silicon wafers: (1) a method in which cleaning is conducted using a diluted hydrogen fluoride solution, (2) a method in which cleaning is conducted using a mixed solution of either hydrochloric acid or sulfuric acid and hydrogen peroxide, and (3) a method in which cleaning is conducted using a mixed solution of ammonia and hydrogen peroxide. The cleaning liquid used in each of these cleaning methods contains water and a highly pure form of chemicals designed to maximize the reduction of minute particle contaminants and transition metal contaminants.

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Among the previous methods noted above, method (1) is capable of dissolving a natural oxide film with a normal thickness of 10Å on a silicon wafer surface, and while this method is highly effective at removing metallic contaminants within the oxide film, it still presents some difficulty when it comes to reducing the level of minute particle contaminants.

Method (2) is able to use a high level of dissolution capability with respect to the metallic contaminants contained within the sulfuric acid, but it is incapable of dissolving an oxide film. For this reason, it is highly effective when it comes to removing metallic contaminants located on top of an oxide film, but it has very little effect when it comes to removing metallic contaminants that are located within an oxide film or along the interface between an oxide film and silicon.

Since method (3) works to dissolve the silicon itself, it is highly effective at removing metallic contaminants located on top of the silicon layer. However, due to the fact that the oxide film that is generated within the basic cleaning solution can easily become embedded with the metallic contaminants, etc., that exist within the cleaning solution, there is a high possibility that the silicon wafer will become contaminated once again. However, due to the fact that this method is highly effective at removing minute particles, it is widely used among wafer manufacturers and device manufacturers.

In addition, as a method for resolving the problems experienced with the prior methods noted above, the so-called Slight Etch method was introduced in which a silicon wafer is cleaned by being dipped into a mixed solution of 60 wt% nitric acid and a maximum of 0.1 wt% hydrogen fluoride. (Ritsuo Takizawa, et al., "Extended Abstracts of Solid State Devices and Materials, 1988, P. 475)

However, highly pure nitric acid, which is referred to as semiconductor grade nitric acid, still contains ppb-order or sub-ppb-order metallic contaminants such as AI, Ca, Cu, Fe, K, Na, Zn, etc. Accordingly, there is a high concentration of metallic contaminants within cleaning solutions that contain a high concentration of nitric acid, such as 60 wt%. Furthermore, when a cleaning tank made of quartz glass is used, the metallic impurities within the quartz glass become eluted into the solution, causing the concentration to gradually increase.

Also, with the high oxidation strength of highly concentrated nitric acid, an oxide film forms on the surface of silicon wafers, and the metallic contaminants within the cleaning solution can easily become

embedded within this oxide film. Therefore, even when the Slight Etch method is applied, there is a limit to the level of high purification that takes place with regard to the silicon wafers.

Problem to Be Solved by the Invention

A method for evaluating the purity of silicon wafer surfaces is one in which the lifetime (hereinafter referred to as the recombination lifetime) is investigated using the microwave reflection method. Using this method, the inventors have evaluated the purity of silicon wafers that were cleaned according to each type of method available. The results showed that in cases where Fe is included in the cleaning solution during cleaning operations in which a mixed solution of ammonia and hydrogen peroxide is used, contamination occurs along the silicon wafer surface at a level of approximately 8 x 10¹¹ atoms/cm² even when the Fe amount is very low at 0.5 ppb. It is further understood that this causes a drop in the recombination lifetime. (Otsuka, et al., The 34th Semiconductor and Integrated Circuit Technology Symposium, Preliminary Findings, 1988, P. 37)

The objectives of this invention are as follows: to significantly reduce the level of minute particle contaminants as well as metallic contaminants such as Fe when cleaning silicon wafers; to eliminate quality problems such as the occurrence of defects along the oxidation inductive lamination layer, as well as drops in lifetime; and to obtain a highly pure silicon wafer that will prevent degradation of electrical properties when used in devices.

An outline of this invention follows.

- (1) A method for cleaning a silicon wafer is characterized by a cleaning liquid comprised of an aqueous solution that contains 0.1 20 wt% hydrogen fluoride during the silicon wafer cleaning process, along with 0.5 25 wt% nitric acid that is used as an oxidizing agent.
- (2) A method for cleaning a silicon wafer is further characterized by a cleaning liquid comprised of an aqueous solution that contains 0.05 10 wt% hydrogen fluoride during the silicon wafer cleaning process, along with 0.05 10 wt% hydrogen peroxide that is used as an oxidizing agent.
- (3) A method for cleaning a silicon wafer is further characterized by a cleaning liquid comprised of an aqueous solution that contains 0.05 10 wt% hydrogen fluoride during the silicon wafer cleaning process, along with oxidizing gas bubbles that are mixed into the solution to be used as an oxidizing agent.

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This invention is designed to minimize the amount of additives for the purpose of significantly reducing the level of impurities in a cleaning solution when a cleaning operation is conducted for silicon wafers. In addition, a cleaning solution with a superior level of cleaning capability is used. Specifically, this invention calls for an oxidizing agent to be added to a highly acidic aqueous solution containing a minimal amount of fluorine ions. Furthermore, as the oxide film along the silicon wafer surface is dissolved, an etching capability is provided for the silicon, making it possible to effectively remove metallic contaminants such as Fe, etc. Claim (1) notes that a minimal amount of nitric acid is used as an oxidizing agent, whereas Claim (2) notes that a minimal amount of hydrogen peroxide is used, and Claim (3) notes that an oxidizing gas is used.

According to this invention, the respective concentrations of hydrogen fluoride, nitric acid, and hydrogen peroxide within the cleaning solution are given in weight percentages of HF, HNO₃, and H₂O₂. In Claim (3), it is possible to use an oxidizing gas that contains oxygen as well as nitrous oxide (dinitrogen monoxide). Furthermore, an ultrapure form of water is used as a solvent.

In Claim (1), given less than 0.1 wt% of hydrogen fluoride and less than 0.5 wt% of nitric acid, the removal effect with regard to the metallic contaminants is insufficient. If the hydrogen fluoride concentration is increased to exceed 20 wt%, a trend is recognized in which the amount of minute particle contaminants increases along the surface of the silicon wafers. Furthermore, if the nitric acid concentration is increased to exceed 25 wt%, there is an excessive amount of etching along the silicon surface, resulting in a defective wafer surface with a cloudy appearance. Thus, if the maximum concentration of hydrogen fluoride is set to 20 wt% and the maximum concentration of nitric acid is set to 25 wt%, there is no substantial problem with regard to the concentration of impurities that become intermixed from the chemicals.

Therefore, the concentration of hydrogen fluoride has been set to a range of 0.1 - 20 wt%, and that of nitric acid has been set to a range of 0.5 - 25 wt%. Note that if the cleaning solution temperature is allowed to increase beyond the required level, this will cause the hydrogen fluoride as well as the water and nitric acid to escape in the form of steam and may result in a cleaning solution that falls outside the scope prescribed by the invention. Furthermore, increasing the temperature requires more time, which could result in a significant loss of productivity. Therefore, the preferred maximum temperature is 80° C.

In Claim (2), given less than 0.05 wt% of hydrogen fluoride and less than 0.05 wt% of hydrogen peroxide, the removal effect with regard to the metallic contaminants is insufficient. If the hydrogen fluoride concentration is increased to exceed 10 wt%, a trend is recognized in which the amount of minute particle contaminants increases along the surface of the silicon wafers. Furthermore, if the hydrogen peroxide concentration is increased to exceed 10 wt%, there is an excessive amount of etching along the silicon surface, resulting in a defective wafer surface with a cloudy appearance. Thus, if the maximum concentration of hydrogen fluoride is set to 10 wt% and the maximum concentration of hydrogen peroxide is set to 10 wt%, there is no substantial problem with regard to the concentration of impurities that become intermixed from the chemicals.

Therefore, the concentration of hydrogen fluoride has been set to a range of 0.05 – 10 wt%, and that of hydrogen peroxide has been set to a range of 0.05 – 10 wt%. Note that if the cleaning solution temperature is allowed to increase beyond 80°C, this will cause uneven cleaning such that pits may form on the silicon wafer surface after the heat treatment is conducted. Therefore, the preferred maximum temperature is 80°C.

In Claim (3), given less than 0.05 wt% of hydrogen fluoride and no intermixing of oxidizing gas bubbles, the removal effect with regard to the metallic contaminants is insufficient. If the hydrogen fluoride concentration is increased to exceed 10 wt%, the amount of minute particle contaminants increases along the surface of the silicon wafers, and at the same time, the etching amount becomes excessive, resulting in a defective wafer surface. Thus, if the maximum concentration of hydrogen fluoride is set to 10 wt%, there is no substantial problem with regard to the concentration of impurities that become intermixed from the chemicals. Furthermore, since a highly pure form of an oxidizing gas can be relatively easily obtained which has a very low concentration of impurities, this poses no problem.

Therefore, the concentration of hydrogen fluoride has been set to a range of 0.05 – 10 wt%, and oxidizing gas bubbles are intermixed to be used as an oxidizing agent. Note that if the cleaning solution temperature is allowed to increase beyond 80°C, this will cause uneven cleaning such that pits may form on the silicon wafer surface after the heat treatment is conducted. Therefore, the preferred maximum temperature is 80°C.

In order to intermix the oxidizing gas bubbles within the cleaning solution, it is possible to use a means that is already well-known, such as inserting a gas introduction tube into the cleaning tank or installing gas jets along the bottom of the cleaning tank such that the gas is allowed to bubble into the tank.

Based on this invention, there is an electrochemical coupling between the anodic dissolution reaction of the silicon that occurs between the silicon and fluorine ions, and the cathodic reaction that is caused by the oxidizing agent, resulting in a movement of the corrosion potential to the anode side. This makes it easy to remove the metallic contaminants from the silicon wafer surface.

Passive membranes comprised of silicon oxides are either chemically or electrochemically dissolved within the highly acidic aqueous solution containing fluorine ions that fall within the scope of the method discussed in this invention. Due to the fact that this will cause stripping of the silicon wafer surface, it is necessary to add a certain amount of oxidizing agent, and when the corrosion potential moves to the anode side, the metal contaminants are easily removed from the wafer surface.

Note that according to the method described in this invention, substances other than those noted above as components of the cleaning solution may also be added without causing a loss of cleaning capability. Examples include salt types such as ammonium fluoride, etc.

In addition, according to the method of this invention, it is also acceptable to use prior well-known forms of cleaning methods in conjunction with this method. As an example, for greater effect, cleaning can be conducted using a mixed solution of ammonia and hydrogen peroxide, followed by another cleaning in which a diluted fluorine aqueous solution is used, after which cleaning is finally conducted using the method of this invention.

Embodiments

<1> Embodiment for Claim 1

The surfaces of silicon wafers are contaminated with the following: approx. 270 x 10¹⁰ atoms/cm² of Cr, approx. 240 x 10¹⁰ atoms/cm² of Cu, approx. 2230 x 10¹⁰ atoms/cm² of Fe, and approx. 313 x 10¹⁰ atoms/cm² of Ni. These wafers are then dipped into the various cleaning solutions listed in Table 1, which provides the results for each cleaning. Immediately after cleaning, the silicon wafers are cleaned twice for at least five minutes each under ultrapure running water, after which they are spun dry and an analysis is conducted to determine the level of metallic contamination on the surface.

During the analysis, chemical etching using a concentrated fluorine and nitric acid solution is applied to dissolve a 1 μ m surface layer, after which the metallic element concentration within this solution is measured using a frameless atomic absorption photometry analysis method. Note that ND indicates a level that falls below the lower limit for analytical determination. Also note that Cr is less than 0.1 x 10^{10} atoms/cm², Cu and Fe are less than 0.2×10^{10} atoms/cm², and Ni is less than 2.0×10^{10} atoms/cm².

The minute particles on the wafer surface are measured using a wafer surface particulate measuring device, and those wafers showing 10 particulates per wafer or less are indicated with an O, whereas those showing more than 10 particulates per wafer are indicated with an X.

In addition, a visual judgment is made as to whether the wafer surfaces after cleaning are hydrophobic or hydrophilic. Those that are hydrophobic are indicated with an O, those that are slightly hydrophobic are marked with a Δ , and those that are hydrophilic are marked with an X. A hydrophobic surface indicates that a silicon oxide, namely and oxide layer, does not exist on the silicon wafer surface.

An optical microscope is then used in order to observe whether or not there are any pitting defects along the wafer surface, and the findings are included in the table. The absence of pits indicates that the etching amount is appropriate, such that the wafer has an extremely smooth mirror surface.

In Table 1, Comparison Examples 1 and 15 show that the residual amounts of Fe and Cu are particularly high due to the low levels of hydrogen fluoride during cleaning. In the same fashion, Comparison Examples 6 and 14 show a high occurrence of pitting as well as residual minute particle contamination due to the fact that the hydrogen fluoride levels are too high. Pitting defects also occur in the cases of Comparison Examples 19 and 20 due to the fact that the nitric oxide levels are too high.

Prior Art Example No. 21 in which the Slight Etch cleaning method is applied uses an aqueous solution that has 60 wt% of HNO3 and 0.1 wt% of HF, but the removal effect is low with regard to Fe. Prior Art Example No. 22 in which the Ammonia Hydrogen Peroxide cleaning method is applied uses an aqueous solution that has 4.1 wt% of NH₃ and 4.4 wt% of H₂O₂, and among the various cleaning methods, this one has the lowest removal effect with regard to metallic contaminants; especially in the case of Fe. Prior Art Example No. 23 in which the Chlorine Hydrogen Peroxide cleaning method is applied uses an aqueous solution that has 5.1 wt% of HCl and 4.4 wt% of H₂O₂, and although this method is currently the most widely used due to its metallic contaminant removal effect, it still has a low removal effect with regard to Fe when compared to the examples given for this invention.

Example (1) of this invention shows a significant reduction in both minute particle contaminants as well as metallic contaminants, with no evidence of pitting defects on the surface after cleaning. Furthermore, the

surface is shown to be hydrophobic after cleaning, with no existence of an oxide film. This means that the type of recontamination that occurs when cleaning is performed in such a way that an oxide film is formed during cleaning and metallic contaminants within the cleaning solution are allowed to become embedded within the oxide film has not occurred in the case of Example 1 of this invention.

<2> Embodiments for Claims 2 and 3

The surfaces of silicon wafers are contaminated with the following: approx. 18 x 10¹⁰ atoms/cm² of Cr, approx. 110 x 10¹⁰ atoms/cm² of Cu, approx. 110 x 10¹⁰ atoms/cm² of Fe, and approx. 21 x 10¹⁰ atoms/cm² of Ni. These wafers are then dipped into the various cleaning solutions listed in Table 2, which provides the results for each cleaning. The cleaned wafers then undergo the same procedures as noted in Embodiment <1> with regard to water rinsing and drying, followed by an analysis of the metallic contaminants, measurements regarding minute particle contaminants, and observations of pitting defects. The results are shown in Table 2.

Examples (2) and (3) of this invention, which are the respective embodiments of Claims (2) and (3) of this invention, show that the levels of metallic contaminants and minute particle contaminants are drastically reduced, with no evidence of pitting defects.

Due to the low levels of hydrogen fluoride and hydrogen peroxide used during cleaning in the case of Comparison Example No. 8, as well as the low level of hydrogen fluoride used during cleaning in the case of Comparison Example No. 9, both of these examples show high residual amounts of Cr, Cu, and Fe. In the case of Comparison Example No. 15, the low level of oxidizing agent used during cleaning results in high residual amounts of Cr, Cu, and Fe. Also, as shown in Comparison Examples No. 16, No. 17, and No. 18, excessive amounts of hydrogen fluoride and hydrogen peroxide result in the appearance of pitting defects as well as an increase in the level of minute particle contaminants.

Table 1

			Third	Clean-		Heavy	metal co	ontaminat	ion on			• •	
	HNO ₃	HF	Com-	ing	Sol.		urface aft			Surface	·	Min.	·
No.			ро-	Time	Temp.		(x 10 ¹⁰ at	oms/cm ²)). ·	After	Pitting	Part.	Class.
	(%)	(%)	nent '	(sec.)	(°C)					Cleaning	Defects	Cont.	
	· · ·		(NH ₄ F)			Cr	Cu	Fe	Ni				
01	0.50	0.05	None	300	25	61	2.3	23	ND	X	None	0	CE
02	0.10	0.10	None	300	25 ·	2.4	20	. 15	ND	Δ	None	· 0 ·	CE
03	0.50	5.00	None.	300	25	ND	ND	ND	ND	0	None	. 0	PE1
04	0.50	10.0	None	300 .	25	ND	ND.	ND	ND	0	None	0	PE1
05	0.50	20.0	None	300	25	ND	ND.	ND	ND	O.	None	. 0	PE1
06	0.50	30.0	None	300	25 .	ND	ND	ND	ND	0	Yes	X.	CE
07.	0.50	5.00	0.1%	300	25	ND .	ND	ND	ND	O.	None	. O	PE1
08	0.50	5.00	None	300	40	ND ·	ND	ND ·	ND	. O .	None	0	PE1
09	0.50	5.00	None	300	60	ND	ND	ND.	ND	O.	None	0	PE1
10	0.50	5.00	None	300	80	ND ·	ND	ND.	ND	0	None	O	PE1
1.1	15.0	0.10	None	300	25	ND	ND	· ND	ND	.0.	None	0 ·	PEI
. 12	15.0	0.10	0.1%	300	25	ND	ND	ND .	ND	0	None	0	PE1

	150	20.0	None	300	. 25	ND	ND	ND	ND	0	None	0	PE1
13	15.0	20.0	None		· 25								
14	15.0	30.0	None	300	25	ND	ND	ND	ND	0	Yes	<u>X</u> .	CE
15	25.0	0.05	None	300.	25	ND	1.8	. 3.3	ND_	X	None	0	CE
16	25.0	0.10	None	300	25 ,	. ND	ND	ND	ND	. 0	None ·	Ο.	PE1
17	25.0	· 5.00	None	300	25	ND.	ND	ND.	ND	0	None	0	PE1
18	25.0	10.0	None	300	25	ND	ND	ND	ND	0	None	· O	PEI
19	30.0	5.00	None	300	· 25	ND	ND	ND	ND	0	Yes	O	CE ·
20	30.0	20.0	None	300	25	ND	ND	· ND	ND	0	Yes	Ο.	CE
21	Sligh	nt Etch M	ethod	300	70	ND	2.8	34	ND	X	None	0	PAE
22		onia Hyd		600	80	2.7.	. 2.4	77	'ND	X	None	0	PAE
		oxide Me									,	,	
23	Chlo	rine Hyd	rogen	600	· 80	ND	ND	15	ND	X	None	O	PAE
•	•	oxide Me						<u> </u>	<u> </u>				

[Translator's Note: In the Classification (Class.) column above, CE = Comparison Example; PE1 = Patent Example (1); PAE = Prior Art Example]

Table 2

			 			T avi							
0-			Oxidiz	:				•	ontaminat				
				Third	Clean-				er cleanir				·
			ing	Com-	ing	Sol.		(x 10° at	oms/cm²)		D	Min.	
No.	HF	H_2O_2	Gas	ро-	Time	Temp.			•	•	Pitting	Part.	Class.
	•		Com-					}	1				1
	(%)	(%)	posi-	nent	(sec.)	(°C)				^	Defects	Cont.	
			tion	·			Cr	Fe	Ni [.]	Сυ			! "
			(%)										222
01	0.05	1.00	None	None	600	25	ND	ND	· ND	· ND	None	0	PE2
02	0.51	0.10	None	None	600	25	ND	ND	ND	ND	None	0	PE2
03	0.10	2.01	None	None	600	25	ND:	ND	ND	ND	None	.0	PE2
04	0.50	0.12	None	None	600	25	ND_	ND	ND.	ND	None	O	PE2
05	1.05	0.11	None	None	360	25	ND	ND	ND	. ND	None	0	PE2
.06	1.00	1.07	None	NH ₄ F	240	25	ND	ND	ND	ND	None	Ο	PE2
				0.10%	•	· .			<u> </u>				
07	0.99	5.00	None	None	120	25	ND	ND	ND	. ND	None	O	PE2
08	0.03	0.04	None	None.	600	25	8.2	6.8	ND	5.3	None	. O ·	CE
09	0.01	1.00	None	None	600	25	ND	23.4	ND.	12.4	None	0	CE
10	0.10	0.20	None	None	600	40	ND	ND ·	ND	ND	None	0	PE2
11	0.05	None	Pure O ₂	None	600	25	ND	ND	, ND	ND ·	None	0	PE3
12	0.15	None	80%O ₂ + 20%Ar	None	600	25	ND	ND	ND	ND	None	О	PE3
13 -	1.01	None	20%O ₂ +80%N ₂	NH ₄ F	360	. 30	ND	ND	ND	, ND	None	. 0	PE3
14	0.02	None	Pure O ₂	0.10% None	360	25	. ND	45.8	ND	7.9	None	· O	CE
15	0.15	0.01	None	None	600	25	· ND	12.4	ND	8.4	None	0	CE
. 16	11.0	2.05	None	None	600	25 .	ND .	ND	ND	ND	None	X	CE
. 17	5.95	10.2	None	. None	600	25 ·	ND	ND	ND	ND	Yes	. O	CE
18	11.2	None	Pure O ₂	None	600	25	ND	· ND	ND	ND	Yes	X	CE
19	1.00	None	20%N ₂ O + 80%N ₂	None	600	30	ND	ND	ND	ND	None	0	PE3

[Translator's Note: In the Classification (Class.) column above, CE = Comparison Example; PE2 = Patent Example (2); PE3 = Patent Example (3)]

Effect of the Invention

When a silicon wafer is cleaned using the method described in this invention, a highly pure silicon wafer can be obtained in which the levels of metallic contaminants and minute particle contaminants are significantly reduced. Furthermore, not only does this invention make it possible to avoid a drop in quality among silicon wafers, such as the occurrence of defects along the oxidation inductive lamination layer as well as a drop in lifetime, when these wafers are used in highly integrated devices such as IC, LSI, etc., it is also possible to prevent degradation of electrical properties in these devices.

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